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# **Experimental Determination of Interface Trap Density and Fixed Positive Oxide Charge in Commercial 4H-SiC Power MOSFETs**

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**ABSTRACT** We measure interface trap density near the conduction band edge and fixed oxide charge in commercial, packaged, 4H-SiC 1.2 kV planar Power MOSFETs. These traps determine the device threshold voltage, performance, and reliability. The subthreshold slope is used to extract interface trap density at the SiO<sub>2</sub>-SiC interface near the conduction band edge from three vendors, which varies from  $5.8 \times 10^{12}$  to  $9.3 \times 10^{12}$  cm<sup>-2</sup>·eV<sup>-1</sup>. Good agreement is obtained with threshold voltage measurements from 25°C to 150°C as devices with the highest interface trap densities exhibit the largest threshold voltage reduction over temperature. Fixed positive oxide charge,  $N_{ot}$ , balanced with interface traps and substrate doping, varies from  $3.3 \times 10^{12}$  cm<sup>-2</sup> to  $3.7 \times 10^{12}$  cm<sup>-2</sup>. At high temperatures, electrons captured in interface traps emit to the conduction band and lower the threshold voltage together with fixed oxide charges, which are as high as interface trap densities. Thus, device design should be considered for a suitable threshold voltage to ensure the device does not operate in a Normally-ON condition and to protect against gate voltage surges. Therefore, more focus on characterization and reduction of the interface trap density and fixed oxide charge is needed to enable further improvement in effective electron mobility of SiC MOSFETs.

**INDEX TERMS** Silicon carbide (SiC), power MOSFET, oxide reliability, interface trap density, oxide charge, subthreshold slope, threshold voltage.

# I. INTRODUCTION

SiC Power MOSFETs are efficient switching devices with low switching losses and high-power density over an extended temperature range [1]–[3]. SiC, similar to Si, uses thermally grown silicon dioxide (SiO<sub>2</sub>) as a native oxide. However, the gate oxide of SiC MOSFETs exhibits a higher density of trapped charges at or near the SiC-SiO<sub>2</sub> interface. The high density of electrons in the interface traps ( $D_{it}$ ) near the conduction band edge, along with fixed positive charges,  $N_{ot}$ , near the SiC-SiO<sub>2</sub> interface create a design challenge for threshold voltage and cause reduced electron density in the conduction band. Furthermore, scattering of electrons in the channel results in a low effective electron mobility, a reduced current drive, and an increase in channel and ON resistance [4]–[7]. Post-oxidation annealing (POA)

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techniques with nitric oxide (NO), nitrous oxide (N<sub>2</sub>O), phosphosilicate glass (PSG), and phosphorus oxychloride (POCl<sub>3</sub>) have been employed to improve gate oxide quality and increase inversion electron mobility by passivating the SiC-SiO<sub>2</sub> interface [8]–[16]. Recently, Kobayashi *et al.* [17] and Takichi *et al.* [18] have reported new approaches to reduce  $D_{it}$  and improve effective mobility by preventing oxidation of SiC during gate oxide formation.

The combination of extremely low intrinsic carrier density combined with p-base doping places the Fermi level near the conduction band edge in strong inversion, where the high values of  $D_{it}$  affects the threshold voltage and device reliability. The issues arising from the high  $D_{it}$  become complex when devices with dissimilar  $D_{it}$  operate at elevated temperature. Electrons trapped by interface traps emit back into the conduction band. This results in an uneven threshold voltage reduction and current drive. In a power module, where multiple devices are connected in parallel to share the



current, the uneven threshold voltage reduction in paralleled devices results in uneven current sharing. The nonuniform current sharing can affect the long-term reliability of power modules. Even with reduction of  $D_{it}$ , the electron mobility is degraded by the scattering from the high density of fixed positive charges near the SiC-SiO<sub>2</sub> interface. Although the origin of oxide charge has not been determined, a SiC-SiO<sub>2</sub> transition layer with carbon clusters formed during the thermal oxidation process may be responsible for the donor-like defects [19]–[22].

In our work, we determine  $D_{it}$  and  $N_{ot}$  in commercially available 1.2 kV SiC Power MOSFETs. Transfer current-voltage (*I-V*) characteristics in the subthreshold region are used to extract the  $D_{it}$  near the SiC conduction band edge, which are confirmed with high temperature measurements of the device threshold voltage. We extract  $N_{ot}$  for an assumed p-base doping density.

# II. EXTRACTION METHOD FOR $D_{it}$

In order to examine the trap density at the interface of  $SiO_2$ -SiC, we use the subthreshold characteristics. This permits the extraction of energy-dependent trap density by incorporating the surface potential derived from the subthreshold characteristics. We begin with the drain current in the subthreshold region [23], [24]

$$I_{DS} = I_0 e^{\frac{qV_{GS}}{nkT}} \left( 1 - e^{\frac{-qV_{DS}}{kT}} \right) = I_{DM} e^{\frac{q\phi_S}{kT}} \tag{1}$$

where  $I_0$  is the current at  $V_{GS} = 0$  and  $V_{DS} \gg kT/q$ .  $I_{DM}$  is the maximum drain current at zero surface potential ( $\phi_S = 0$ ) which incorporates  $V_{DS}$ . The ideality factor n is given as

$$n = \frac{q}{2.3kT} \left(\frac{\partial log I_{DS}}{\partial V_{GS}}\right)^{-1} = \frac{dV_{GS}}{d\phi_s} = 1 + \frac{C_D + C_{it}}{C_{ox}} \quad (2)$$

where  $C_D$  is the depletion capacitance,  $C_{ox}$  is the oxide capacitance and  $C_{it}$  is the interface trap capacitance per unit area with the interface trap density

$$D_{it}\left(\phi_{s}\right) = \frac{C_{it}}{q} \tag{3}$$

In practice,  $D_{it}$  is extracted at several gate voltages, as a function of surface potential, within the subthreshold region. Fig. 1 shows the energy band diagram under weak inversion where the Fermi level  $(E_F)$  is slightly above the intrinsic Fermi level at the surface  $(E_{iS})$ .

The traps in the range  $E_F - E_{iS}$  are filled with electrons and this range extends as the applied gate voltage increases to bring  $E_F$  closer to the conduction band at the surface,  $E_{CS}$ . The onset of inversion at  $\phi_S = 2\phi_F$  places the  $E_F$  near the edge of  $E_{CS}$ , where there is an increasing density of interface traps. The amount of the interface charge varies as the surface potential changes with the gate voltage. The surface potential is related to trap level,  $E_{TO}$ , by the following expression:

$$E_{CS} - E_{T0} = \frac{E_g}{2} - q \left( \phi_s - \phi_F \right) \tag{4}$$

where  $\phi_F$  is the Fermi potential. Both  $\phi_S$  and  $\phi_F$  are positive quantities in (4). The drain current value at a certain gate

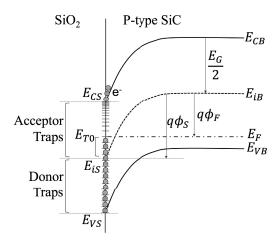


FIGURE 1. Energy band diagram of the SiC-SiO<sub>2</sub> system in weak inversion.

voltage at a fixed value of  $V_{DS}$  can be expressed as the last term in (1). The threshold voltage is set at  $\phi_S = 2\phi_F$  in (1), such that

$$I_{DS}\left(2\phi_F\right) = I_{DM}e^{\frac{2q\phi_F}{kT}} \tag{5}$$

Combining (1) and (5) leads to  $\phi_S$  with the current level  $I_{DS}$  ( $\phi_S$ ) measured at a certain gate voltage as

$$\phi_s = 2\phi_F - 2.3 \frac{kT}{q} log \frac{I_{DS} \left(2\phi_F\right)}{I_{DS} \left(\phi_S\right)} \tag{6}$$

where the surface potential is in the range  $\phi_F < \phi_S < 2\phi_F$ .  $I_{DS}$   $(2\phi_F)$  is the drain current at threshold voltage which is determined by the linear extrapolation method from the measurement data. Finally, from (4) and (6),  $E_{CS} - E_{T0}$  is expressed as a function of surface potential:

$$E_{CS} - E_{T0} = \frac{E_g}{2} - q \left( \phi_F - 2.3 \frac{kT}{q} log \left[ \frac{I_{DS} \left( 2\phi_F \right)}{I_{DS} \left( \phi_S \right)} \right] \right) \tag{7}$$

# **III. EXPERIMENTAL RESULTS AND DISCUSSION**

# A. INTERFACE TRAP DENSITY DISTRIBUTUION EXTRACTION

We examine commercial SiC planar power MOSFETs. The devices under test (DUTs) are from three vendors, referred to as C, D, and E, which are rated at 1.2 kV and 7 – 12 A. Five devices from each vendor are selected with threshold voltage variation less than 0.05 V. All the electrical characterizations are performed with a Keysight B1505A analyzer. Fig. 2 shows  $I_{DS}-V_{GS}$  characteristics with a drain voltage of 0.1 V at room temperature. Threshold voltage at  $\phi_S = 2\phi_F$  is determined by a linear extrapolation (LE) method [25]. From the subthreshold curves, the ideality factors n can be determined with (2) as a function of  $V_{GS}$ . Several gate voltages are selected in the subthreshold region.  $D_{it}$ , as a function of trap energy, is obtained with (3) and (7). To determine  $C_{ox}$ , oxide thicknesses are estimated by voltage ramp-to-breakdown measurements at room temperature as shown in Fig. 3. With an oxide breakdown field of 11 MV/cm [26], [27], DUT oxide

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thickness, from vendors C, D, and E, are 456, 452, and 389 Å, respectively. A p-type base doping concentration,  $N_A = 2 \times 10^{17}$  cm<sup>-3</sup> has been assumed for all samples.

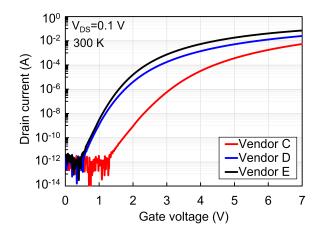


FIGURE 2.  $I_{DS}$ - $V_{GS}$  transfer characteristics at room temperature.

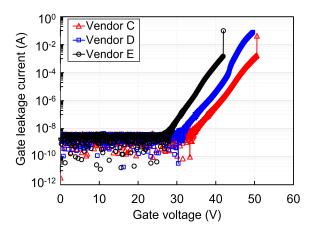


FIGURE 3. Voltage ramp-to-breakdown (V-ramp) measurements on DUTs.

Fig. 4 shows a sensitivity analysis of the extraction of interface trap density with varying p-base doping concentrations and oxide breakdown fields which affect the estimated gate oxide thickness. A small error can be incurred with this method since the p-base doping profile is not known for each vendor.  $D_{it}$  distributions of devices from vendors C, D and E are shown in Fig. 5. For each vendor,  $D_{it}$  distributions of five devices are overlapped which shows a small deviation across the devices from the same vendor. The  $D_{it}$  increases exponentially near the conduction band edge. The channel electrons are captured and scattered by these interface traps during device operation and their effective mobility is reduced, which decreases the drive current since SiC Power MOSFETs operate in the region  $E_{CS} - E_{T0} \leq 0.1$  eV, where  $D_{it}$  is high. At  $E_{CS} - E_{T0} \cong 0.1$  eV, where inversion occurs, the average  $D_{it}$  values from the vendors C, D and E are  $9.3 \times 10^{12}$ ,  $6.8 \times 10^{12}$ , and  $5.8 \times 10^{12}$  cm<sup>-2</sup> · eV<sup>-1</sup>,

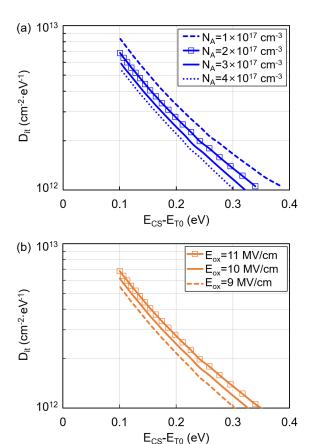


FIGURE 4. Sensitivity analysis of interface trap density with varying (a) p-base doping concentration and (b) oxide breakdown field (vendor D).

respectively. Vendors D and E might have very similar interface trap distribution since there can be a variation in p-base doping concentrations whereas vendor C appears to be quite different even at deeper energy levels. The post oxidation anneal (POA) of the gate oxide plays a role in determining the  $D_{it}$ . Studies on the SiO<sub>2</sub>-SiC interface demonstrate N<sub>2</sub>O and NO anneal work best for the Si-face of 4H-SiC, which has been used in industry [28], [29]. N<sub>2</sub>O and NO treated MOS capacitors, compared with simply oxidized MOS capacitors, exhibited approximately 83 percent and 90 percent lower  $D_{it}$  at 0.1 eV below the conduction band, respectively [29]. Our  $D_{it}$  values are higher than reported values in [29] since the DUTs are commercial MOSFETs with heavily implanted Al p-base regions.

# B. TEMPERATURE-DEPENDENT THRESHOLD VOLTAGE

Threshold voltages are measured as a function of temperature in order to study the performance of DUTs with different  $D_{it}$  values at high temperature. The devices were placed in an oven and measured at 25°C intervals from room temperature to 150°C.  $I_{DS}$ – $V_{GS}$  transfer characteristics as a function of temperature are shown in Fig. 6 (a). As the temperature increases, the curves shift in the negative direction in all samples. Noticeable difference in subthreshold characteristics

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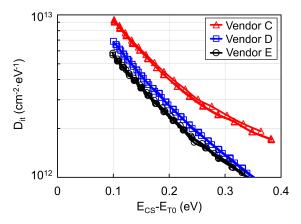


FIGURE 5. Extracted energy-dependent interface trap density distribution.

between vendors is observed. Subthreshold swing (SS) which is the inverse slope of the log ( $I_{DS}$ ) versus  $V_{GS}$  in the subthreshold region, is a simple indicator for  $D_{it}$ , as shown in (2) and (3).

Generally, the SS is higher in devices with larger  $D_{it}$ , which shows a gradual subthreshold slope. Fig. 6 (a) shows devices from vendor C present gradual subthreshold slopes with larger shift in  $I_{DS}-V_{GS}$  curve over the given temperature range whereas subthreshold slopes of devices from vendor E are steep and shift over the temperature is smaller. This indicates devices from vendor C have higher  $D_{it}$ . Vendor D is not shown for clarity but is located between the two vendors with medium subthreshold slope. Fig. 6 (b) shows the threshold voltage reduction with temperature. Devices from vendor C show the largest variation in threshold voltage with the temperature change as expected from the variation in I-V curves in Fig. 6 (a). High threshold voltage at  $150^{\circ}$ C for vendor C may be seen as an advantage from the point of view of safe operation of the circuit.

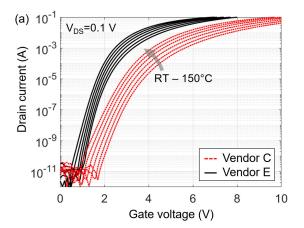
When threshold voltage at room temperature is taken as a reference, the threshold voltage reductions at 150°C in devices from vendors C, D, and E are 3.4 V, 2.6 V, and 1.7 V, respectively. The threshold voltage reduction at high temperature is primarily due to release of trapped electrons in interface states to the conduction band. The threshold voltage is defined as

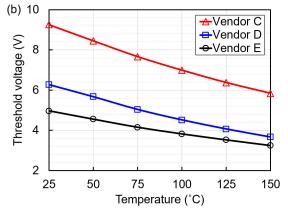
$$V_{TH} = \phi_{GS} + 2\phi_F + \frac{\sqrt{4\epsilon_s q N_A \phi_F}}{C_{ox}} - \frac{Q_{it}}{C_{ox}} - \frac{Q_F}{C_{ox}}$$
 (8)

Consequently, the less negative charges in the interface traps and more carriers in the conduction band result in threshold voltage reduction. Threshold voltage reduction from room temperature to 150°C,  $\Delta V_{TH}$ , can be described

$$\Delta V_{TH} \cong \frac{\Delta Q_{it}}{C_{ox}} \tag{9}$$

where variations in  $Q_F$  with temperature is assumed to be small. The first three terms in (8) involve temperature changes





**FIGURE 6.** Temperature-dependent (a)  $I_{DS}$ - $V_{GS}$  transfer characteristics and (b) threshold voltages.

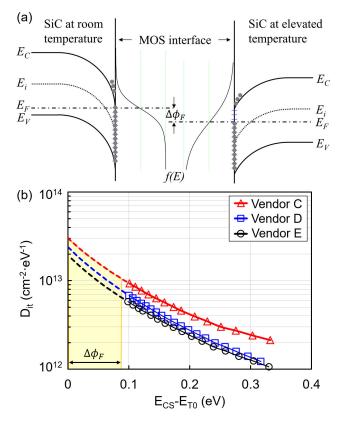
due to  $\phi_F$  and bandgap narrowing and amount to threshold voltage reduction of only 0.19 V, 0.19 V, and 0.18 V for vendors C, D and E, respectively. Thus, the threshold voltage shift in experimental data is assumed to largely come from the emission of trapped charges in interface states. Interface traps per unit area,  $\Delta N_{it}$ , can be expressed as

$$\Delta N_{it} = \int_{\phi_{F,HT}}^{\phi_{F,RT}} D_{it} \left( \phi_F \right) d\phi_F = \frac{\Delta V_{TH} C_{ox}}{q}$$
 (10)

where the threshold voltage is determined at  $\phi_S = 2\phi_F$ . The Fermi potential change  $(\Delta\phi_F)$  from room temperature  $(\phi_{F,RT})$  to 150°C  $(\phi_{F,HT})$  is depicted in Fig. 7 (a) [30]. At elevated temperature,  $E_F$  is closer to the  $E_i$  at the bulk due to increasing intrinsic carrier density. Therefore, less band bending is required to induce a sufficient carrier density in the conduction band at the surface. Trapped electrons above the  $E_F$  emit back to the conduction band by the amount of Fermi potential change which results in fewer negative charges at the interface.  $\Delta\phi_F$  is the same for all samples as 0.085 V since we assume the same p-base doping for all DUTs. The effect of Fermi-Dirac distribution broadening at high temperature is neglected in the calculation.

 $N_{it}$  can be calculated by two methods, either by integrating  $D_{it}$  within the potential change using the  $D_{it}$ 

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**FIGURE 7.** (a) Fermi potential difference at room temperature and elevated temperature are shown in energy band diagrams at  $\phi_S = 2\phi_F$  with temperature-dependent Fermi-Dirac function f(E) and (b) Extended interface trap density distribution towards the conduction band edge.

distribution obtained in the previous section A (method A), or from temperature-dependent threshold voltage reduction (method B). Table 1 shows the extracted  $N_{it}$  values from two methods.  $N_{it}$  extracted from method B is indeed the integration of  $D_{it}$  from the conduction band edge where  $E_F$  locates at room temperature ( $E_{CS} - E_{T0} \cong 0$  eV) to  $\Delta \phi_F$  ( $E_{CS} - E_{T0} \cong 0.085$  eV).

Therefore, in order to integrate  $D_{it}$  from the conduction band edge through  $\Delta\phi_F$ , method A has been further extended to estimate  $D_{it}$  in the strong inversion.  $I_{DS}$   $(2\phi_F)$  in (7) is raised close to the inversion point,  $E_{CS} - E_{T0} \cong 0$  eV.  $N_{it}$  from method A in Table 1 is the integrated areas under each  $D_{it}$  curve in Fig. 7 (b).  $N_{it}$  values extracted from both the techniques are in good agreement.

The number of fixed charges per unit area,  $N_{ot}$  (= $Q_F/q$ ), is also calculated from (8) by subtracting the contribution of interface charges at room temperature. Here we assumed that the negative trapped charges within 0.3 eV of the conduction band contribute most of the negative charge in  $N_{it}$ . Therefore, integration is performed from  $E_{CS}$  to  $E_{CS}$  – 0.3 eV for each vendor in Fig. 7. The value assumed for the p-base doping  $N_A$  is 2 × 10<sup>17</sup> cm<sup>-3</sup> as mentioned previously. Extracted  $N_{it}$  and  $N_{ot}$  values from DUTs are summarized in Table 1.

TABLE 1. Extracted  $N_{it}$  and  $N_{ot}$  values from DUTs.

Number of Traps (/cm²)		Vendor C	Vendor D	Vendor E
$N_{it}$	Method A	1.5×10 <sup>12</sup>	1.2×10 <sup>12</sup>	$9.2 \times 10^{11}$
	Method B	1.5×10 <sup>12</sup>	1.2×10 <sup>12</sup>	8.6×10 <sup>11</sup>
$N_{ot}$		5.6×10 <sup>12</sup>	4.8×10 <sup>12</sup>	4.4×10 <sup>12</sup>

Although this method may provide relative comparison between devices and across the vendors, extracted values are not highly accurate compared to the real values since occupied trap density,  $N_{it}$ , is unlikely to be zero at  $T=150^{\circ}\mathrm{C}$ . Therefore, our experimental condition gives a lower bound on  $N_{it}$  and  $N_{ot}$ .

## IV. CONCLUSION

We describe a method to extract interface trap density,  $D_{it}$ , and oxide trap density,  $N_{ot}$ , on 1.2 kV commercial, packaged 4H-SiC Power MOSFETs. There is a delicate balance between the interface and oxide trap densities together with the design of the impurity profile to meet performance and reliability at room and elevated temperatures. These devices are under consideration for electric vehicles (EVs) and solar energy applications.

A subthreshold slope method, combined with temperature measurements of threshold voltage, is used to determine the above-mentioned trap densities, as shown in Table 1. Since process information is often not available from vendors, in our studies we estimated a gate oxide thickness with rampto-breakdown measurement and assumed a p-base doping of  $2 \times 10^{17}$  cm<sup>-3</sup>. The results in Table 1 indicate the significant differences among three vendors. Five devices, each from three different vendors C, D, and E, are used in the study. For example, a threshold voltage reduction over a temperature range from 25°C to 150°C of 3.4 V for vendor C is correlated with the highest integrated interface trap density. In terms of device operation, under fast switching with high switching losses, increasing junction temperatures cause a negative shift in threshold voltage. The threshold voltage should be carefully chosen to be higher than a critical value for safe operation of the circuit.

At high temperatures, electrons trapped in interface states emit to the conduction band and lower the threshold voltage together with fixed oxide charges, which are as high as interface trap densities. Thus, the impurity profile must be adjusted to maintain a threshold voltage to ensure the device does not operate in a Normally-ON condition and to protect against gate voltage surges. Therefore, more focus on characterization and reduction of the interface trap density and fixed oxide charge is needed to enable further improvement in effective electron mobility of SiC MOSFETs. Moreover, in high power applications where multiple MOSFETs are paralleled within a power module and multiple power modules are used, current sharing across devices should be uniform for long-term reliability. Otherwise, devices with

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low threshold voltage will carry a larger share of the total current.

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